Cooling Connections Testing and Development: Progress Report

September 28, 2000

N. Hartman, E. Anderssen, M. Gilchriese, T. Weber, F. Goosen, J. Taylor, J. Wirth

Current Cooling Connections - Permanent Options

Adhesive Bonding

- 6061 Aluminum fittings at demountable breaks and sector terminations
- 3003 Aluminum sector tubing and exhaust tubing
- Capillary material unknown
- Hysol 9396 adhesive has been used 9394 may also be desireable
- Electrical breaks created by PEEK inserts

Brazing

- 6063 Aluminum fittings at demountable breaks and sector terminations
 - higher melting point than 6061
- 3003 Aluminum sector tubing and exhaust tubing
- Capillary material unknown
- Two braze techniques have been tried
 - · vacuum furnace brazing
 - hand torch brazing
- Metallized alumina pieces used to create electrical breaks

Current Cooling Connections - Demountable Options

Custom Aluminum Fittings

- 6061 or 6063 machined fittings
 - low mass
 - shaped for either braze or adhesive joint geometry (see subsequent slide)
- Standard O-ring type groove
- Custom split clamp
 - low profile and low mass
 - · prevents unwanted torque

Standard Seals

- UHMWPE face seal with SS internal spring -Variseal Brand (www.variseal.com)
- O-ring compatible groove
- Also consistent with all-metal Wills C-ring type gasket





Permanent Connections - Adhesive Bonding

Types of Joints

- Rectangular (sector) to round (fitting) tube terminations
 - sector tubing is 4.67 x 2.30 mm outer dimension (hydraulic diameter is 2.39 mm)
 - fitting is 4.43 mm ID x 5.50 mm OD (round)
 - requires an intermediate rectangular to round transition piece
- Capillary to fitting junctions
 - small capillary bonded into larger round fitting
 - exhaust tubing is 5.50 mm OD (hydraulic diameter is 4.43 mm)
 - requires an intermediate adaptor piece (in order to use the same fittings)
- Exhaust tube to fitting junctions
 - exhaust tube is 5.50 mm OD (hydraulic diameter is 4.43 mm)
 - requires no adaptor bonds directly into fitting

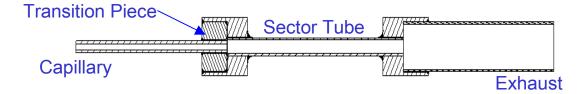
Adhesives

- Hysol 9396 (baseline used for all tests so far)
- Hysol 9394 (aluminum filled version of 9396 may be more rad hard)

Adhesive Bond Samples

- Test piece models all three connections (but no electrical breaks)
 - Sector termination
 - rectangular to round transition
 - Capillary Termination
 - small to large diameter transition
 - Exhaust Termination







- Samples prepared for several tests
 - Pressure testing
 - Irradiation
 - Thermal cycling
 - Black anodized to simulate worst possible bond

Adhesive Bond Test Setups



Fas-Test Fitting Setup

Pressure Testing

- Tested at 100 psi (6.5 bar) using Fas-Test fittings
- Pressurized with N2 gas pressure decay measured
- Tested before and after irradiation.

Irradiation

- Samples exposed to 3 Mrad in liquid C3F8
- Leak rates measured before and after irradiation
- Thermal cycling will also be tested



C3F8 Pressure Vessel

Acceptable Leak Rates

- Meaningful leak rate specification must be defined in order to conduct any sort of testing
- Decision must be made as to how much C3F8 contamination is acceptable in detector volume
- Rough estimate of leak rate spec was made for comparison purposes only:
 - Assume allowable mass leak is 1 kg per 100 days = 125 L @ STP, and that system pressure is 1 bar gauge = 760 Torr
 - Estimate 100 sectors and 100 staves (each circuit is equivalent to 1 test piece) = 200 circuits total; assume that there are 2x200 circuits in pixel thermal volume (including demountable fittings) + 100 fittings = 500 total
 - These assumptions arrive at an approximate leak rate of 2 x 10⁻⁵
 Torr-Liters/sec for each circuit (test piece)

Pixel Detector

Adhesive Bond Pressure Test Results

- 10 Samples made for irradiation 10 samples made for thermal cycling
 - Irradiation samples tested before and after
 - Thermal cycling samples tested before (cycling is not yet complete)

Test	Avg. Leak Rate Before	Avg. Leak Rate After	Passing Samples (Before)	Passing Samples (After)
Condition	Torr-L/se c	Torr-L/se c	(Out of 10)	
Irradiation	8.51E-06	2.79E-06	10	2
Thermal Cycling	1.22E-04	NA	4	NA

Test Implications

- Only positive leak rates were averaged into above table
- Many test pieces showed pressure gain with time this means that either the test equipment is too susceptible to noise, or that the test fixture was leaking high pressure gas into the fittings
- Of the 14 tests that "failed" only 3 actually registered leak rates above the nominal leak rate spec (the remaining samples showed pressure "gain")
- Samples that passed (16 of 30 tests) showed high factors of safety (above 10 on average)

Permanent Connections - Brazing

Types of Joints

 Joint geometries are identical to those examined for adhesive bonding, except that clearances must be changed for brazing

Braze types

- Furnace Braze
 - Foil situated in the joint, between concentric tubes
 - foil made in house at LBNL, rolled to 25-100 microns thick
 - Al-Si eutectic created, with 1% Mg added to aid wetting
 - · Braze paste placed in and around joint area
 - Commercially available paste with no Mg
 - Mg must be supplied through atmosphere to aid wetting
 - Furnace cycle run in dry N2 or Argon

Hand Torch Braze

- Paste in and around joint (pre-mixed with flux)
- Wire around edge of joint (with flux) contains Mg for wetting
- Use oxy-acetylene or propane torch

Permanent Connections - Brazing cont.

Braze fittings

- Since braze success was uncertain, simple mock fittings were made for testing
- Two types of fitting were made, each with two different clearances
 - close fit 50 micron radial gap for wire and paste brazing
 - loose fit 100 micron radial gap for paste, wire, and foil brazing

Tests

- Samples were cleaned with NaOH prior to brazing
- All brazes were Helium leak checked after brazing and cleaning
- The following braze test combinations were attempted (# brazes)

TORCH	Foil	Wire		Paste
Close Fit	0		4	2
Loose Fit	0		0	2
FURNACE	Foil	Wire		Paste
Close Fit	0		0	(
Loose Fit	2		0	2

Brazing Results - Furnace

Furnace brazing turned out difficult to control

- Temperatures could not be kept even along the part as well as desired (about 10 degrees variation)
- Wetting was not very substantial
- Surface quality on components cycled in furnace were variable (perhaps due to overheating)



Failed Paste Braze



	Foil	Wire	Paste
Close Fit	0	0	0
Loose Fit	0/2	0	1/2



Successful Paste Braze

Brazing Results - Torch

- Torch results are good for certain geometries
 - Melting of the parts was not a problem
 - Wetting was not very substantial - but filleting could be easily achieved
 - Surface quality at overheated areas was poor - need to simply use care in application of torch



Successful wire fillet braze

He Leak Tight Brazes

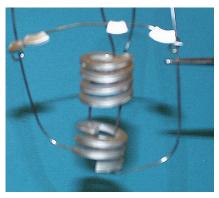
	Foil	Wire	Paste
Close Fit	0	4/4	0/2
Loose Fit	0	0	1/2



Porous but leak tight paste braze

Corrosion Tests on AI in C3F8

- Sector Tubing (3003) was placed in liquid C3F8 and irradiated to 3
 Mrad
 - Two sample sizes
 - Large coil approximately 1.5 grams
 - Small section approximately 0.05 grams
 - Samples were held off of the bottom of containment vessel with SS wire, in order to insure complete contact with C3F8
 - Masses were measured with high precision balance numerous times on different days and averaged

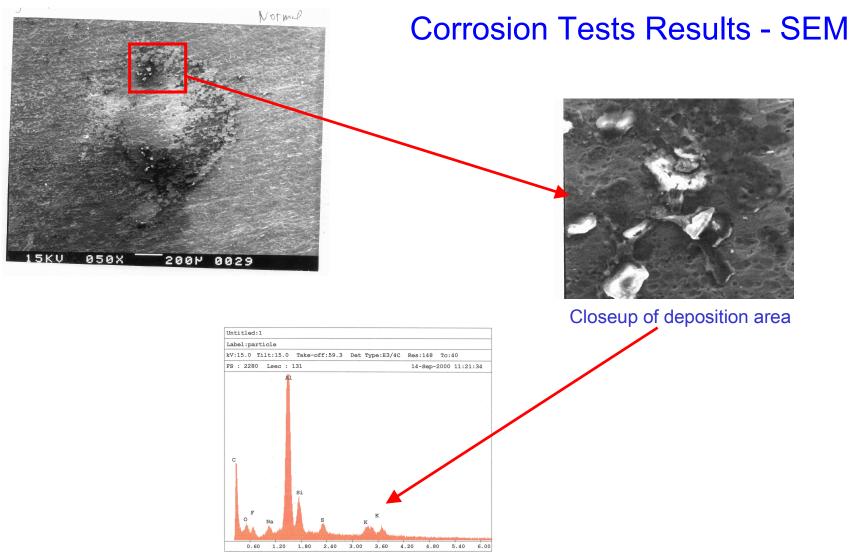


Large coil suspended by SS wire

Corrosion Tests Results

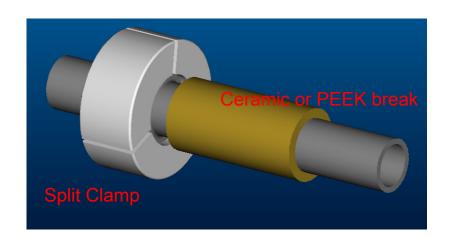
- After 3 Mrad exposure some small changes were observed
 - Most samples appeared to gain mass
 - small samples about 1 part in 100,000 on par with the standard deviation of our measurements
 - large samples about 1 part in 10,000 approximately 10 times our resolution
 - Samples were examined with SEM in order to check this mass increase, and to look for corrosion
 - evidence of F and C was found by mass spectrometer indicates some sort of polymerization
 - · no sign of corrosion or attack on the aluminum was observed
- Since results are sensitive but significant, more testing will be conducted
 - Continue to irradiate current aluminum samples to 6 Mrad total
 - Use same C3F8 as before, which was captured after first irradiation cycle

Pixel Detector



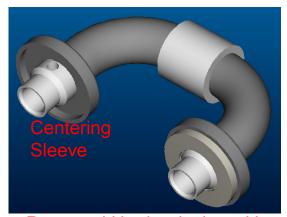
Mass Spec results show evidence of polymerization and cleaning agents

Proposed Real Sector Fittings

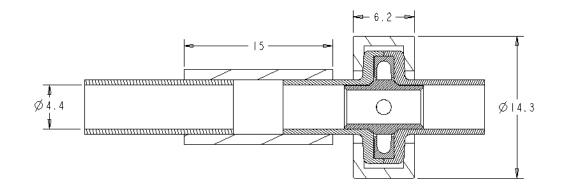




Proposed swage on end of sector tubing



Proposed U-tube design with electrical break



Summary

- Adhesive bonded sector terminations work well and pass our initial leak rate spec estimation
 - Need to fix problems with leak check tests pressure gain should not be seen, so we may need different appartus (perhaps with more sensitivity)
 - Need to test the split clamp demountable fittings (may eat up leak budget)
 - Need to recheck irradiated samples (many more will most likely pass our spec once we iron out test technique)
 - Helium leak check all terminations for comparison
 - Must complete thermal cycling tests
- Brazed sector terminations have shown mixed results
 - Furnace brazing is time consuming and hard to control, and results have not been good
 - Torch brazing is fast and inexpensive, but results with paste and foil are not good
 - Torch brazing with wire (fillet style) is effective need to make new termination geometries that are conducive to fillet brazing and test

Summary Cont.

Corrosion of AI in C3F8 was not observed

- Mass gain was measured with larger samples
- SEM shows carbon and fluorine in deposition areas
- Need to irradiate further to demonstrate clear trend
- Should test carbon panels in same manner (may see more polymerization)

Demountable fittings must still be tested

- Leak checking has begun, but few samples have been made
- Need to prototype all joints in their proposed forms
- Ceramic or PEEK electrical break must be fabricated and tested

General Work Needed

- Demountable Fittings
- Meaningful Leak Spec
- Capillary terminations in actual material
- Corrosion/polymerization potential for carbon/plastics